

Kinetics of a Three-Step Isomerization of Glucose to Fructose Using Immobilized Enzyme

M. H. Gaily, A. K. Sulieman, and A. E. Abasaheed

Abstract—A three-step complex formation of fructose by glucose isomerization was suggested to describe the isomerization kinetics. The model was characterized by the formation of a fructose complex. Experimental data obtained from the isomerization process using immobilized Sweetzyme enzyme, IT® were used in this study. Experiments were conducted at different reaction temperatures in the range of 50-70°C and glucose initial concentrations of 10, 15 and 20% and enzyme loading of 1g. Glucose concentrations dropped with time until equilibrium was reached. A first order kinetics for the steps was employed and Runge Kutta 4th order algorithm combined with a least square method were used to estimate the pre-experimental factor and activation energy for determination of the corresponding rate constants by solving the initial value problem of the suggested model using EZ-Solve software. Very good fits between experimental data and model prediction was obtained.

Index Terms—Fructose, glucose, isomerization, kinetics.

I. INTRODUCTION

Fructose, an isomer of glucose, is used commercially in foods and beverages industry. It is a simple sugar found in many foods and has a high relative sweetness. It is the sweetest of all naturally occurring carbohydrates and is 1.73 times the sweetness of sucrose [1]. Interest in converting glucose to fructose has attracted the attention of researchers who concentrated their efforts towards maximizing fructose yield and minimizing the costs of all associated processes [2].

Isomerization of glucose to fructose, a reversible reaction catalysed by an enzyme, is a very important industrial process to produce high fructose syrup. This enzyme was discovered in the mid of the nineteenth century and called glucose isomerase and its systematic name is d-xylose ketol-isomerase EC 5.3.1.5 [3].

Industrially, starch (a glucose polymer) is the most commonly used feedstock for production of fructose. The process depends on hydrolysing the starch into highly concentrated glucose syrup which is further processed in the presence of an isomerase. A typical process for production of fructose syrups uses alpha-amylase to liquefy starch and then

glucoamilase to saccharify the hydrolyzed starch for the content of 94% dextrose. This resulting product will be directed for isomerization [4]. Since the conversion of glucose to fructose is equilibrium limited, the amount of fructose produced by the enzymatic isomerization reaction is related to the equilibrium constant of the reaction. A simpler purification process, based on isomerases immobilized on solid supports after the hydrolysis reaction were reported. Such processes have the advantage of reutilizing the isomerase [5], [6].

Glucose to fructose isomerization is initiated by protonation of the C2-OH and the formation of a furanose aldehyde intermediate. Fructose is produced via a hydride transfer from C2 to C1 on the furanose aldehyde followed by the rehydration of the C2 carbocation [7].

Different Models by different researchers on glucose isomerization to fructose in fluidized bed reactors were reported in the literature [8] – [15]. From the kinetic point of view, glucose to fructose isomerization is a reversible reaction that is characterized by formation of an intermediate complex [16], [17].

Kinetics of fructose-glucose isomerization in a recirculation reactor was studied [18], where Pseudo-first order kinetics was proposed in the temperature range 303-333 K, pH 7.5 and initial concentrations 0.5-2 mol/l. A generalized linear model for glucose isomerization by immobilized isomerase that satisfactorily represented the experimental data was reported [19].

Immobilized glucose isomerase from *Streptomyces murinus* was used in a packed bed reactor to obtain fructose from glucose and the kinetics of the isomerization is reported [20]. Also, in another study [21], glucose isomerization and fructose separation in the presence of cation-exchanged zeolites (A, X and Y zeolites) and hydrotalcites zeolites exchanged with moderate basicity (NaX and KX) achieved isomerization of glucose to fructose with 90% selectivity to fructose but at low glucose conversions (10-20%). Synthesized catalysts were also used for isomerization of glucose to fructose, such process was carried out over as-synthesized Mg–Al hydrotalcite (HT_A), calcined Mg–Al hydrotalcite (HT_C), and rehydrated Mg–Al hydrotalcite (HT_R) catalysts and it was found that rehydration process served an efficient method for increasing the catalytic performance of hydrotalcite in the isomerization of glucose into fructose [22].

The kinetics and equilibrium of isomerization reaction of D-glucose to D-fructose have been investigated using a commercial immobilized glucose isomerase (IGI), Sweetzyme type IT®, in a batch stirred-tank reactor to

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predict the concentration profiles of D-glucose and D-fructose within the reactor. The experimental results indicated that the model prediction of the transient and steady-state performance of the packed-bed reactor was satisfactory and as such could be used in the design of a fixed-bed IGI catalytic reactor [23].

In this contribution, the reaction scheme was assumed to go through two intermediate complexes; the first is a glucose-enzyme complex and the second is a fructose-enzyme complex. The kinetic investigation covers of 10-20% initial glucose concentrations and 50-70°C reaction temperature. An algorithm coupled with a least square method was developed to determine the relevant kinetic parameters.

II. MATERIALS AND METHODS

Three different glucose solutions of 10, 15 and 20% were prepared separately by weighing 10, 15 and 20 grams of pure glucose, respectively, and dissolving in 100 ml deionized water. 1 gram of immobilized enzyme, Sweetzyme IT® obtained free of charge from Novozyme Company, Denmark was placed in a perforated support at the bottom of the packed bed reactor as shown in Fig. 1. A peristaltic pump was used to recirculate the glucose solution over the immobilized enzyme in the packed bed reactor at a rate of 8ml/second. The reactor was equipped with a temperature-controlled water heating jacket to maintain the temperature of the sugar solution within ± 0.1 °C of operating temperature. Isomerization temperatures of 50, 60 and 70 °C were used with each sample. Duplicate experiments were performed.

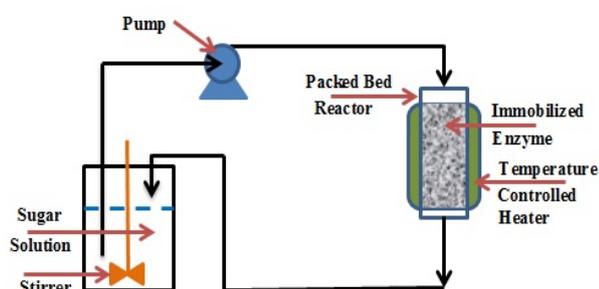


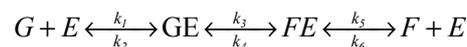
Fig. 1. Schematic diagram of the experimental set-up

Samples were analyzed for sugars concentration each two hours using High Performance Liquid Chromatograph, HPLC (Agilent 1100 series, model G1362A) equipped with IR detector. Agilent Silica based- Zorbax carbohydrate column, 4.6 mm ID x 150 mm (5 μ m) was used for separating and identifying, qualitatively and quantitatively glucose and fructose in the samples collected during the isomerization process. The column temperature was set at 35°C. 70:30 vol. % of acetonitrile in deionized water was used as a mobile phase at a flow rate of 1.5 ml/min.

III. RESULTS AND DISCUSSIONS

Glucose isomerization was assumed to proceed via a three-step process that involves the formation of two complexes (glucose-enzyme and fructose-enzyme) as shown

below.



where G =glucose; F =fructose; E =enzyme; GE =glucose-complex; FE =fructose complex.

k_1 , k_3 and k_5 are the forward reaction rate constants for first, second and third steps respectively.

k_2 , k_4 , and k_6 are the backward reaction rate constants for first, second and third steps respectively.

The kinetic investigation covered a reaction temperature range of 50 - 70°C and initial glucose concentrations ranging from 10% - 20%. The model assumes reversible first order kinetics for the three steps. The rate constants associated with the model and the corresponding activation energies and pre-exponential factors are evaluated using Runge Kutta 4th and the least square method for minimization of errors. Rate constants are assumed to follow Arrhenius expression, i.e.,

$$k_i = k_{i0} e^{-\frac{E_i}{RT}}$$

The activation energy (E_i) can be obtained from the slope of the graph when $\ln(k_i)$ is plotted against $(1/T)$; the pre-exponential factor (k_{i0}) can be obtained from the intercept of the same equation.

A. Model Development

$$-\frac{d(G)}{dt} = k_1(G)(E) - k_2(GE) \quad (1)$$

$$\frac{d(GE)}{dt} = k_1(G)(E) - (k_2 + k_3)(GE) + k_4(FE) \quad (2)$$

$$\frac{d(FE)}{dt} = k_3(GE) - (k_4 + k_5)(FE) + k_6(F)(E) \quad (3)$$

Let:

$$K_3 = \frac{k_1}{(k_2 + k_3)} \quad \text{and} \quad K_4 = \frac{k_4}{(k_2 + k_3)}$$

$$L_3 = \frac{k_3}{(k_4 + k_5)} \quad \text{and} \quad L_6 = \frac{k_6}{(k_4 + k_5)}$$

Applying the quasi-steady state assumption for the two complexes, i.e.,

$$\frac{d(GE)}{dt} = 0 \quad \text{and} \quad \frac{d(FE)}{dt} = 0;$$

Equations (2) and (3) become:

$$K_3(G)(E) - (GE) + K_4(FE) = 0 \quad (4)$$

$$L_3(GE) - (FE) + L_6(F)(E) = 0 \quad (5)$$

Solving e (4) and (5) simultaneously, gives:

$$(GE) = \frac{[K_3(G) + K_4 L_6 (F)](E)}{(1 - K_4 L_3)}$$

And

$$(FE) = \frac{[L_3 K_3 (G) + L_6 (F)](E)}{(1 - K_4 L_3)}$$

$$\text{Let: } M_3 = \frac{K_3}{(1 - K_4 L_3)} \quad \text{and} \quad M_6 = \frac{L_6}{(1 - K_4 L_3)}$$

Substituting into (GE) and (FE) above, gives:

$$(GE) = [M_3(G) + K_4 M_6(F)](E) \quad (6)$$

$$(FE) = [L_3 M_3(G) + M_6(F)](E) \quad (7)$$

Enzyme balance:

$$(E_o) = (E) + (GE) + (FE) \quad (8)$$

Substituting from (6) and (7) into (8), one gets:

$$(E_o) = (E) + [M_3(G) + K_4 M_6(F)](E) + [L_3 M_3(G) + M_6(F)](E)$$

$$(E_o) = [1 + (1 + L_3)M_3(G) + (1 + K_4)M_6(F)](E)$$

$$(E) = \frac{E_o}{[1 + (1 + L_3)M_3(G) + (1 + K_4)M_6(F)]} \quad (9)$$

Substituting (6) and (9) into (1), one gets

$$-\frac{d(G)}{dt} = \frac{[(k_1 - k_2 M_3)(G) - k_2 K_4 M_6(F)]E_o}{[1 + (1 + L_3)M_3(G) + (1 + K_4)M_6(F)]} \quad (10)$$

$$(F) = (G_o) - (G) \quad (11)$$

1) Rate constants estimation

Table I shows the values of the rate constants ($k_1, k_2, k_3, k_4, k_5, k_6$) obtained from data at reaction temperatures of 50, 60 and 70°C using a least square method for parameter estimation. The table, also shows the values of $\ln(k_i)$ and $1/T$

TABLE I: RATE CONSTANTS FOR ESTIMATIONS

T, °C	k1	k2	k3	k4	k5	k6	
50	0.14	0.15	0.11	0.33	0.61	0.69	
60	0.51	0.39	0.29	0.59	0.91	1.13	
70	1.48	0.66	0.75	0.9	2.17	2.1	
T, K	1/TK	ln(k1)	ln(k2)	ln(k3)	ln(k4)	ln(k5)	ln(k6)
323	0.003096	-1.966	-1.897	-2.207	-1.109	-0.494	-0.371
333	0.003003	-0.673	-0.942	-1.238	-0.528	-0.094	0.122
343	0.002915	0.392	-0.416	-0.288	-0.105	0.775	0.742

For each reaction, the activation energy E_i , ($\text{cal.mol}^{-1}\text{K}^{-1}$) and the pre-experimental factor k_{io} , (h^{-1}) can be obtained from the slopes and intercepts of plots of $\ln(k_i)$ versus $(1/T)$. These values are tabulated in Table II.

TABLE II: ACTIVATION ENERGY AND RATE CONSTANT FOR DIFFERENT REACTIONS

Reaction, i	E_i , $\text{cal.mol}^{-1}\text{K}^{-1}$	k_{io} , h^{-1}
1	25974	5.40×10^{16}
2	16350	1.85×10^{14}
3	21124	2.15×10^{13}
4	11057	1.02×10^7
5	13912	1.46×10^9
6	12233	1.28×10^8

B. Overall Predictions

Values of the activation energy E_i , and the pre-experimental factor from Table(2) are used in equation (1) to obtain the corresponding rate constants by solving the initial value problem given by equation (12) using EZ-Solve software. The predictions of the model against corresponding experimental values are illustrated in Figs. (2-4) for initial glucose concentrations of 20%, 15% and 10% and reactions temperatures of 50, 60 and 70°C. As shown by the figures

good agreement is obtained.

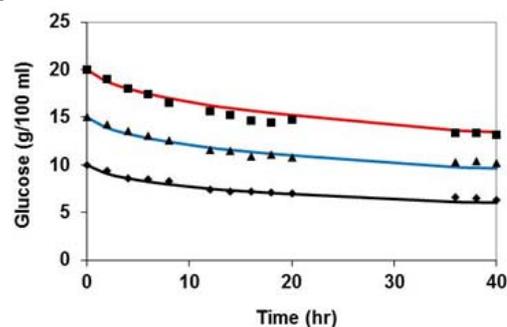


Fig. 2. Comparison of model predictions (solid lines) with experimental values (symbols) at 50°C and at different initial concentrations of glucose (◆=10%), (▲=15%) and (■=20%)

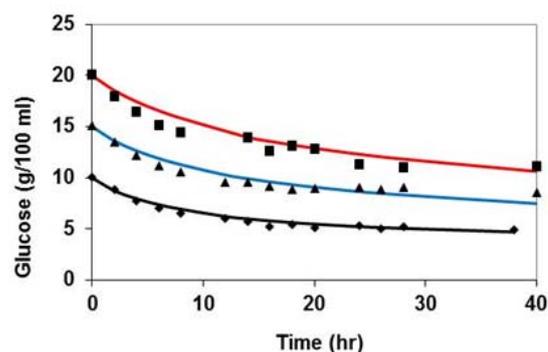


Fig. 3. Comparison of model predictions (solid lines) with experimental values (symbols) at 60°C and at different initial concentrations of glucose (◆=10%), (▲=15%) and (■=20%)

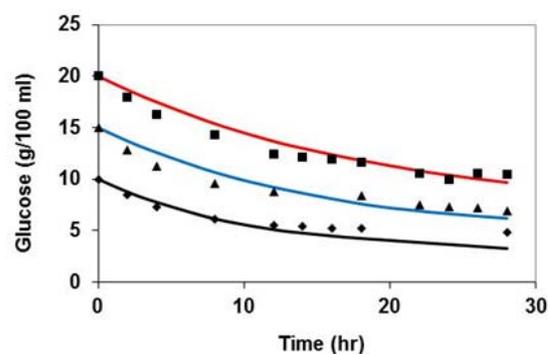


Fig. 4. Comparison of model predictions (solid lines) with experimental values (symbols) at 70°C and at different initial concentrations of glucose (◆=10%), (▲=15%) and (■=20%)

IV. CONCLUSION

Glucose isomerization into fructose reaction was performed in a batch reactor of a fixed working volume of 250 ml using an immobilized isomerase. The reaction conditions covered a wide range of parameters' values: reaction temperatures (50 – 70 °C), initial glucose concentrations (10 – 20%) and initial enzyme loadings (0.5 – 1.5g). Preliminary experiments revealed those reaction temperatures of 40 °C or less requires prohibitively long reaction times and those higher than 70 °C imparts colors on sugar solution due to caramelization. As expected, isomerization of glucose proceeds with reaction time until an equilibrium concentration is reached. Depending on reaction temperatures, the equilibrium position changes; a fact confirmed by the kinetics.

A three-step two-complex kinetic expression that represents a three-step formation of fructose and has six rate constants was suggested and its associated parameters were evaluated using a least square method for minimizing errors.

Reactions as presented are considered to be elementary and follow first order kinetics.

Very good fits between experimental data and model predictions were generally obtained.

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