Removal of Reactive Dye Using Solvent Impregnated Resin

Anjali Awasthi, Sakshi Batra, and Dipaloy Datta

Abstract—In this study, Reactive Blue-13 (RB-13) dye removed by solvent impregnated resin (SIR: Amberlite XAD-7 impregnated with Aliquat-336) at different operation conditions. Batch adsorption studies were dispensed out to gauge the effect of solution pH, dosages, kinetic, temperature, concentration and NaCl salt on the adsorption capacity of the adsorbents. Three kinetic models were chosen to suit the kinetic data: pseudo first order, second order, and intra-particle diffusion. It had been determined that RB-13 dye adsorption followed pseudo-second-order kinetics. Adsorbent SIR was characterized by Fourier transform infrared spectroscopy (FTIR), Scanning electron microscope (FE-SEM) and EDX. Solvent impregnated resin (SIR) was regenerated with 80% (v/v) ethanol aqueous solution for reuse.

Index Terms—Adsorption, aliquat-336, reactive blue-13, XAD-7.

I. INTRODUCTION

In textile industries, it is reported that commonly more than 100,000 dyestuffs with over 7×10^5 tones of dyestuffs (a soluble substance used for coloring that contain various raw materials that remain after dying process, spin-off, diluting agent, etc.) produced yearly [1].

It also found that unexpended dyestuffs are indestructible, non-biodegradable, toxicant and contain various mutagenic and carcinogenic properties. These have an effect on the ecosystem, individuals, aquatic plant and mammal causes various diseases [2]-[4]. A number of studies have pointed out that occurrences of several disease among textile industries staff such as Bladder cancer, Breast cancer, Lung cancer, Oral cavity, and pharynx cancer, nephrosis, skin eruption [5]-[20]. Industrial effluent contains dyes additionally causes such disorders.

So removal of such dyes from industrial effluent could be a challenge to each the textile trade and wastewater treatment facility for treating this effluent. It is compulsory that unused dyes must be removed before discharging the effluent water to the surroundings to evade health hazards and destruction of the scheme.

Major categories for dyes removal are biological, chemical, and physical methods. These methods contain several techniques, Flocculation-Coagulation, adsorption, membrane separation, electrochemical, reverse osmosis, ozone oxidation, and biological treatment etc. Flocculation-coagulation method is not so effective because the dye was produced a multiplex with the flocculant, so removal and recycle of dye causes trouble. Membrane separation and reverse osmosis method are expensive for the economic point of view. Adsorption is one of the best cheap processes for removal of dyes.

The large portion of dyes is Azo Dyes (i.e contain aromatic hydrocarbons). Other classifications done according to the structure of dyes are anionic and cationic dyes. Today reactive dyes are popular among textile industries due to its give permanent coloration to cellulose textile substrates and also color did not fade or discolor on laundering. Various types of reactive dyes used in textile industries depends upon the medium temperature (i.e. Cold brand dye: Dyeing process is carried out at room temperature, Hot brand dye: Dyeing occurs at 60°C, High Exhaust brand reactive dyes: Dyeing process is carried out around 80-90°C). In dyeing process 80% of reactive dye participates for dying the fiber, i.e. 20% remains within the effluent; this is often the hydrolyzed dye that can’t be reused for coloring.

This unused dye remains within the effluent treatment plant. Dye concentrations range 10 – 25 mg/L are cited as being present in dye section effluents [21]. After combining with different effluent streams, the concentration of dyes is more insidious. The limit of the concentration of some cyanogenic dyes in water is 1.0 ng/L.

In this investigation, AmberliteXAD-7 Resin impregnated with Aliquat-336 was prepared for removal of Reactive Blue-13 dye. The effecting parameters such as adsorbent dose, dye concentration, pH, time, temperature and salt concentration on the performance of the adsorption process were also studied. Effect of Concentration was studied and therefore the pseudo-first-order, the pseudo-second-order, and Elovich models were usable to describe adsorption dynamics. Regeneration of SIR was done by 80% (v/v) ethanol aqueous solution, and then reused it up to several times.

The purpose of this study is to shows that the un-used reactive dyes will be removed from the effluent by adsorption process using solvent impregnated resin.

II. MATERIALS AND METHODS

A. Materials

Amberlite XAD-7 resin (20-60 mesh) was equipped by Sigma-Aldrich (Merck, Germany). This nonionic, porous
resin often contains a polyacrylic acid ester group (molecular formula:\[\text{CH}_2\text{CH(COOR)}_n\]). Structure of resin was porous, 80-85Å pore diameter and 380 m\(^2\)/g surface area. Reactive Blue-13 dye contains Azo group (M.Wt.-866.06g/mol; molecular formula-C\(_2\)H\(_8\)ClINa\(_2\)O\(_4\)S\(_2\)) was supplied from Alpha Aesar, Britain. Physical properties and chemical structure of RB-13 dye is shown in Table I and Fig. 1. The stock solution of RB-13 dye was prepared in distilled water (via distillation column, in Material Research Centralized laboratory of MNIT, Jaipur). Analytical reagent (AR)-grade chemicals (Ethanol, HCl, and NaOH) purchased from Merck, India, and Aliquat-336 was purchased from Sigma.

![Chemical Structure of reactive dye Reactive Blue-13.](image)

**Fig. 1. Chemical Structure of reactive dye Reactive Blue-13.**

<table>
<thead>
<tr>
<th>Properties</th>
<th>RB-13</th>
</tr>
</thead>
<tbody>
<tr>
<td>Molecular Formula</td>
<td>C(_2)H(_8)ClINa(_2)O(_4)S(_2)</td>
</tr>
<tr>
<td>Molecular Weight</td>
<td>866.06</td>
</tr>
<tr>
<td>Appearance</td>
<td>Dark Blue</td>
</tr>
<tr>
<td>Solubility (at 20( ^\circ)C)</td>
<td>110 g/L</td>
</tr>
<tr>
<td>Solubility in water</td>
<td>Soluble in water</td>
</tr>
<tr>
<td>Nature</td>
<td>Anionic</td>
</tr>
</tbody>
</table>

**TABLE I: PHYSICAL PROPERTIES OF REACTIVE BLUE-13 DYES**

### B. Preparation of Adsorbent

There are various methods for the preparation of impregnated resin i.e. dry impregnation, wet impregnation etc. We prepared resin by wet impregnation techniques. In this process, the first washing of resin was done with ethanol then with DI water for removal of impurities. For that resin and ethanol mixture was taken in a borosil beaker then put it in magnetic stirrer for 2 hr. After that resin was filtered and filtered resin with DI water put in magnetic stirrer for washing until the pH was neutral. Then the resin was dried overnight in open air after that dried this resin for 12 h in an oven at 313 K. In that case this washed resin impregnated with a certain ratio of Aliquat-336. For the preparation of I Ratio of SIR, 1 gram per 11.28 ml Aliquat-336 in 40 ml hexane was mixed in a flask and placed in a water bath shaker for 24 h (in this study we used 0.25 Ratio of SIR, calculated as per 2.793 ml Aliquat-336 in 40 ml hexane). Hexane was used as a diluting agent for viscous Aliquat-336. Then this impregnated resin was again left overnight in open air for drying, after that, it was kept in an oven at 313 K for 24 h. Then the prepared resin was kept in a desiccator.

### C. Characterization

Characterization of SIR and used SIR (i.e. after adsorption of Reactive Blue-13) was done by using FTIR and FE-SEM. FTIR data was taken in a range of 4000-400 cm\(^{-1}\) by FTIR Spectrum 2 (Perkin Elmer, USA). Different peaks of percentage transmission were studied and analyzed. The surface morphology features of unprocessed, modified and used impregnated resin XAD-7 were observed by Scanning Electron Microscopy (FE-SEM) (Nova NanoSEM 450, Perkin Elmer, USA) and Energy dispersive X-Ray (EDX).

### D. Adsorption Experiments

Batch studies at numerous conditions were performed for determination of adsorption phenomena. The effect of adsorbent dose range 0.01-0.3 g, was studied by taken 10 ml of 50 mg/L dye solution in flask at temperature 303±2 K, and put these flask in water bath shaker for definite time intervals. A kinetic study was done, up to 180 min at an optimum dosage of SIR 0.1 g and an initial concentration of dye solution 50 mg/L. To review the effect of temperature for removal of 50 mg/L dye, experiments were carried out at temperature range 303-333 K. For the study of the effect of NaCl salt on adsorption, 50 mg/L RB-13 dye, 0.1 g dose of adsorbent were taken at a distinct concentration of salt ranges 1000-15000 mg/L for 3 hr at 303 K. So the optimum parameters for the dye removal process was defined by varying one parameter and kept other parameters constant. It was initiate in this study that maximum removal percentage (~99%) of dye was obtained at following optimum parameters 0.1 g dosage, 2 h time, 50 mg/L dye concentration and at 303 K temperature.

The adsorption capacity (\(q_a\)) in mg/g of adsorbent was calculated by the following Equation.

\[
q_a = \frac{(C_0 - C_e)\cdot V}{m_a}
\]

where \(C_0\) (mg/L) is the initial RB-13 dye concentration and \(C_e\) (mg/L) is the equilibrium concentration of the dye, \(V\) (L) is the volume of the dye solution, \(m_a\) (g) is the amount of adsorbent. The removal efficiency was calculated by the following equation.

\[
\text{Removal \%} = \frac{(C_0 - C_e)}{C_0} \times 100
\]

![FTIR analysis of impregnated XAD-7 resin and Impregnated XAD-7 resin after adsorption.](image)

**Fig. 2. FTIR analysis of impregnated XAD-7 resin and Impregnated XAD-7 resin after adsorption.**

### III. RESULTS & DISCUSSION

#### A. Characterization: FTIR Analysis

A Fourier Transform Infrared spectrometer (FTIR)
(NEXUS-650, America) was used to analyze the dominating functional groups on the adsorbent surface. The strong peak around 3439 cm\(^{-1}\) represents the hydroxyl groups -OH, the bond at 2927.4 cm\(^{-1}\) is attributed to the presence of the C-H bond. C-Cl stretching peak shown at 755 cm\(^{-1}\). Bending of O=S=O peak noticed at 598 cm\(^{-1}\). C-C, C-H stretching vibration noticed a sharp peak at 1060.45 cm\(^{-1}\), 2589.3 cm\(^{-1}\). There found a more sharper and higher intensity peak in impregnated XAD-7 resin at 1623.6 cm\(^{-1}\) which shows the presence of –N=N- (Azo) group. Presence of sharper peak at 1543.9 cm\(^{-1}\) and 1046.09 cm\(^{-1}\) shows the presence of N=O group and S=O group in resin.

B. Characterization: FE-SEM Analysis

The physical morphologies and surface properties of the adsorbent were examined by using scanning electron microscopy technique (FE-SEM). Impregnated and used impregnated resin (i.e. after adsorption of RB-13 dye) showed severe differences, a surface of the impregnated resin contained more pores than the surface of used SIR and this results in the higher surface area. It observed from both the Fig. 3(a) and 4(a), that adsorption of RB-13 dye in impregnated XAD-7 resin increases the denseness of the surface. It’s also shown FE-SEM analysis spectrum by the Fig. 3 and 4, that weight % of C, O, Cl was increased after impregnation and there also shows presence of some new components i.e. N, S, Na in used SIR XAD-7 due to adsorption of RB-13 dye. These new elements are present in RB-13 dye structure, so increment in weight % and presence of these new elements confirms the adsorption of RB-13 dyes in impregnated XAD-7 resin surface.

**Impregnated XAD-7 Resin**

**Used Impregnated XAD-7 Resin** (i.e. after adsorption Reactive Blue-13 dye in SIR surface)

**C. Effect of Adsorbent Dosage**

The effect of adsorption dosage on removal of RB-13 dye is shown in Fig. 5. This experiment were performed at various dosage range 0.01 - 0.3 g added to 10 ml of predetermined dye concentration solution 50 mg/L, time 2 hr and temperature 303 K. With increase in adsorption dose there also rise in removal efficiency. At 0.1 g dosage it gives maximum removal of dye ~ 99%. After that increase in (upto
0.3 g) adsorbent dosage there was no change observed in dye removal efficiency. So 0.1 g adsorbent dosage takes as optimum dosage for study of other parameters effect.

**Fig. 5. Effect of adsorbent dosage on adsorption of RB-13 (Initial dye concentration = 50 PPM, t= 2 hr, T= 303 K).**

**D. Effect of Contact Time**

The adsorption kinetics behavior of RB-13 dye onto SIR was studied out up to 180 min, by kept different parameter constant. Fig. 6. shows that the concentration of RB-13 dye reduces from its initial value, so the adsorption capacity of SIR inflated sharply upto the initial 60 min and earned the equilibrium once after 120 min of contact time. Fig. 6 conjointly shows the intra-particle diffusion model, pseudo 1st order adsorption mechanics, pseudo-second order adsorption mechanics respectively. Pseudo-second order adsorption mechanics shows the most effective suited the experimental data as compared to the other adsorption mechanics model.

**Fig. 6. Kinetics of RB-13 adsorption by Impregnated XAD-7 \((m = 0.1 \text{ g}, C_0 = 50 \text{ PPM}, T= 303 \text{ K})\).**

**E. Effect of initial dye Concentration**

Dye concentration effect study was done within the range of 10-500 mg/L range by kept others parameter constant. As shown in Fig. 7. there was sharply increase in dye removal efficiency from 10 to 30 mg/L concentration range, after that up to 30 to 50 mg/L concentration range there was slightly increased in removal efficiency. Then at 50 mg/L concentration its attend equilibrium, and then up to 50 to 500 mg/L concentration range removal efficiency was 99%. At higher concentration range removal was higher. This happened, due to the effect of the concentration gradient. At higher concentration ranges of dyes, there’s usually altogether probability that there was chance of rise in driving force. In order that accumulation of dyes occurs around the adsorption sites.

**Fig. 7. Effect of RB-13 concentration on the % removal \((m = 0.1 \text{ g}, t= 2 \text{ hr}, T= 303 \text{ K})\).**

**F. Effect of pH**

It can be seen that dye reduction efficiency decreases with an increase in hydrogen ion concentration of the solution. At pH 4, reduction efficiency was maximum near about 99% and at pH 12 there was a decrease in removal efficiency. So it’s an outcome that hydrogen ions concentration plays an important role for removal Anionic dye.

**Fig. 8. Effect of pH on % removal of RB-13 \((m = 0.1 \text{ g}, t= 2 \text{ hr}, T= 303 \text{ K})\).**

**G. Effect of Temperature**

Temperature effect studied was done in the varied temperature range 303-333 K. For dye removal process, 303 K temperature was found to be optimum. It absolutely was found that maximum removal of dye was 99 at 303 K and slightly decreases in the removal efficiency of dyes until temperature 333 K., therefore, the result shows that temperature has slightly affected the removal efficiency.
Then this regenerated resin was prepared for reused. Upto 10 min. Then washed resin was oven dried over night. Solution upto 30 min and then again washed with DI water reused after washing with (80 v/v) % ethanol aqueous parameters constant, but there no any change was observed in dye concentration. Then by increase in time duration (upto 180 min), removal efficiency was also changed. So this experiment was performed at 3 hr time, 0.1 g dosage, 50 mg/L dye solution and 1000-15000 ppm salt concentration. It shown by study that as increase in salt concentration dye removal efficiency was also increased.

**H. Effect of Salt**

As express in the various studies, the concentration of sodium chloride salt in dye solution could improve or diminish adsorption rate. Fig. 10 demonstrated the positive consequence of sodium chloride salt on adsorption. It plainly outlined the ascent in color removal efficiency as the concentration of sodium chloride salt in dye solution could improve or diminish adsorption rate. As increase in salt concentration dye removal decreases slightly as increases in temperature. SIR was reused again after regenerated with (80 v/v) % ethanol aqueous impregnated resin is more convenient and beneficial technique.

**I. Regeneration Study**

The used impregnated resin was regenerated with (80 v/v) % ethanol-aqueous solution. Impregnated resin was reused after washing with (80 v/v) % ethanol-aqueous solution upto 30 min and then again washed with DI water upto 10 min. Then washed resin was oven dried over night. Then this regenerated resin was prepared for reused.

**IV. Conclusion**

Solvent impregnation resin has good adsorption capacity for removal of RB-13 dye. Characterization of impregnated XAD-7 resin and used impregnated XAD-7 resin shows adsorption of RB-13 dye due to presence of dye elements. In various parameter effect studies its shows higher removal percent was obtained at lower pH scale. Pseudo-second order kinetic was best fitting kinetic model. At higher concentration, it shows almost 99% removal of dyes. Temperature effect on adsorption symbolized that percentage removal decreases slightly as increases in temperature. SIR was reused again after regenerated with (80 v/v) % ethanol aqueous solution. So removal of reactive dye by solvent impregnated resin is more convenient and beneficial technique.

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**References**


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