Soxhlet Extraction of Crotalaria Juncea Oil Using Cylindrical and Annular Packed Beds

Ratna Dutta, Ujjaini Sarkar, and Alakananda Mukherjee

Abstract—An innovative method for the extraction of vegetable oils, from Crotalaria Juncea seeds, was developed, using suitable solvent in a modified Soxhlet apparatus. The present study describes the general extraction mechanism in modified Soxhlet apparatus and change of mass transfer extent within fixed duration with the change of the shape of packed bed used as a seed holder. Regular cylindrical and annular shaped seed holders were used along with irregular (elliptical) shaped seed holder. Maximization of mass transfer parameter in the up flow regime gave considerable increase in the yield of oil production. Use of annular seed holder gives maximum driving force for the up flow regime and higher mass transfer area, hence improved yield.

Index Terms—Annular packed bed, mass transfer regimes, modified soxhlet extractor, crotalaria juncea oil.

I. INTRODUCTION

Soxhlet based solvent extraction process is the primary means of extracting vegetable oil from oleaginous materials. Crushed oil seeds are put in a packed bed which is in contact with pure solvent for the oil to be transferred from the solid matrix to fluid medium. A particular solvent is chosen, based on the maximum leaching characteristics of the desired solute. The mass transfer that occurs during solvent extraction in a packed column was analyzed [1]-[3]. There is a large amount of work mentioned in the literature [4]-[7], dealing with leaching of bio products from solid with liquid solvents. Bio-oil extracted from Crotalaria Juncea seeds is a promising bio-fuel oil [8]. This promotes the research interest to modify the Soxhlet extraction process [9] in order to maximize the oil yield.

The main objective of this piece of research work is to elucidate the extraction process by experiments to understand the various flow regimes developed during the process and effect of shape of the packed bed on the oil extraction yield by improving extraction rate. Normal cylindrical and annular seed holders along with irregular elliptical filter paper bed were used for comparison. Change of oil extraction rate was also observed by identifying the change of the physical properties of the oil-solvent mixture.

II. EXPERIMENTAL

A. Extraction of Crotalaria Juncea Oil in Modified Soxhlet Apparatus

In this work, solvent extraction was done in a modified Soxhlet apparatus for the production of Crotalaria Juncea oil from the crushed seeds. In a Soxhlet apparatus, the extractor thimble is fitted in between a round bottom flask at the bottom and a bulb condenser at the top. Inside the thimble holder, solid matrix of seeds is wrapped within a packing. Normally, with an appropriate design, the condensed solvent vapour accumulates inside the extractor. Here, the solvent comes in contact with the seeds and oil is leached out. When the condensate moves down through the bed of seeds, mass transfer takes place. However, major amount of mass transfer of oil from the seeds to solvent occurs when the accumulated solvent moves up within the annulus purely due to the hydrostatic pressure head. So combined effect of through circulation and cross circulation of the solvent with respect to the seed bed is reflected in the total extent of mass transfer from solid to liquid. So, surface area offered by the bed and the seed-solvent contact time are the two major factors for the yield of oil production. Generally, seed holders are made by filter paper, having irregular elliptical structure.

In a modified Soxhlet extractor, shape of the seed holders was amended. Regular cylindrical and annular shapes were tried and investigated for finding effect of shape.

Both modified seed holders were made by wire-mesh having one end sealed. Cylinder shaped holder had ID: 5 cm, OD: 5.4 cm and length: 33 cm whereas annular shape had two cylinders, with outer one having same dimension as before and the inner cylinder had ID: 2 cm and length: 33 cm. Annular portions was used to hold seeds. These seed holders can be accommodated in a standard Soxhlet extractor having a solvent capacity of 3lt. All the experimental runs were carried out for a duration within which three times siphoning out of solvents occurred. At the end of a batch run, the packed bed of seeds was removed and afterwards the oil-solvent mixture is distilled further by simple batch distillation followed by separation of the mixture using a rotary evaporator apparatus (Make: BUCHI; Model: Rotavapor R-3). The extractions were performed in triplicate and their mean values and standard deviations were calculated. The percentage yield is calculated on the basis of the following equation with \( W_1 \) being the amount of seed taken in gm and \( W_2 \) being the amount of oil produced in gm.

\[
\% \text{ Oil Yield} = \left( \frac{W_2}{W_1} \right) \times 100.
\]

Oil yield in two cases using regular cylindrical seed holder and annular seed holder were compared with normal irregular shaped elliptical bed (made by filter paper).

III. THEORY

A. General Extraction Mechanism

More or less three distinct mass transfer steps are to be
followed during extraction of oil from plant seeds [10], [11]: a) transport of the oil component through the pores of the matrix (intra-particle diffusion), b) diffusion through the stagnant liquid film present outside the solid seed (external diffusion) and c) removal of the oil component from a solid matrix by thermodynamic partitioning into the adjacent flowing solvent.

Importance of the steps is judged by noting the variation of extraction yield with change of condensed solvent flow rate, solvent volume and contact time. If the intra-particle diffusion step is controlling one, then extraction rate and yield will not depend on bulk solvent flow rate. If extraction is controlled by external film transfer diffusion, extraction rate increase with solvent flow rate. On the other hand, where the extraction is controlled by thermodynamic partitioning, doubling the bulk fluid flow rate would double the extraction rate.

Since, in a Soxhlet extractor bulk solvent flow rate is available due to flow of condensed solvent at isothermal condition, so; superficial velocity in the bed remains same in all runs but interstitial velocity through the bed may be varied due to variation in porosity of the bed. Bed porosity can be varied only by varying size fraction of the crushed seeds. Mass transfer controlling step can be chosen in the down flow regime by varying porosities of the bed and that can be used for determining the controlling step for the overall mass transfer. Since down flow regime is short on duration; up flow regime will offer major share in obtaining the amount of mass transfer which solely depends thermodynamic partitioning with external mass transfer.

B. Two flow Regimes within Soxhlet Extractor: Qualitative Analysis

In Soxhlet extractor, condensed solvent falls on the bed, which aids the extraction (at its boiling point temperature) at isothermal and isobaric condition. Mass transfer occurs during two circulations of the solvent; firstly, by downpour of the solvent and secondly, by up flow of the solvent under hydrostatic pressure head. These two mass transfer regimes are acting in series combination and yield of oil production greatly depends on duration of the specific regimes and mass transfer area available in both the cases.

2) Effect of specific surface area of solid substrate in bed

Specific surface area of solid substrate in bed acts as mass transfer area for oil transfer in the first regime. Specific surface area of a solid substrate particle in a packed bed \((a_p)\) is generally describes the ratio of effective inner area of the bed for mass transfer to total volume of the bed. From the Fig. 1 and Fig. 2, it is evident that keeping same outer radius, change of the effective bed radius changes effective surface area of solid substrate for mass transfer. In cylindrical shaped bed, inner area is function of \(R_1\) only; but, in annular shaped bed, it is function of \((R_1 - r)\). Hence in order to accommodate same amount of seeds, higher bed height was approached in annular shaped seed holder, giving lower \(a_p\) value with the same porosity of the bed. This area, \(a_p\) determines the amount of mass transfer in down flow regime only. Obviously, as \(a_p\) increases, rate of mass transfer increases, hence yield of oil production increases. Though, \(a_p\) was more in normal cylindrical bed, but effect of that on oil yield was not so great because of shorter duration of that regime compared to the total extraction time (Table II).

3) Effect of shape of the bed

Specific surface area of the bed acts as the mass transfer area for oil transfer during up flow of solvent. Shape has great effect on specific surface area of solid bed \((a_s)\), which has significant role in changing the yield of oil production. Two regular shapes of seed holders were used in this work and their performance (based on yield of oil production) were compared with traditional irregular elliptical shaped filter paper bed. Since, \(a_s\) is the mass transfer area for up flow regime, so as this increased, rate of mass transfer increased and gave higher yield. Combined effect of higher \(a_s\) and higher duration of up flow regime (since bed height is higher) gave highest yield in case of the use of annular shaped seed holder. In normal cylindrical seed holder, one cylindrical surface area having radius 2.7 cm and 13.7 cm height was acting \(a_s\). But, in annular seed holder, two cylindrical surface areas were available; one having radius 2.7 cm, height 21.3 cm and second having 1 cm radius and 21.3 cm height. Experimentally, it was found (reflected in Table II) that the
regular annular shaped bed works most efficiently though its performance is somewhat offset by lower $a_x$ and lower interstitial velocity.

**TABLE II: EFFECT OF SHAPE OF SEED HOLDER ON OIL YIELD**

<table>
<thead>
<tr>
<th>Bed Shape</th>
<th>Bed height, L (cm)</th>
<th>$a_x$ ($cm^2$)</th>
<th>$a_{y*}$ ($cm^2$)</th>
<th>Down flow duration (sec)</th>
<th>Up flow duration (sec)</th>
<th>Interstitial velocity (cm/sec)</th>
<th>Oil yield (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Elliptical (Irregular)</td>
<td>16.1</td>
<td>-</td>
<td>-</td>
<td>65</td>
<td>2160</td>
<td>0.0135</td>
<td>2.95</td>
</tr>
<tr>
<td>Cylindrical (Regular)</td>
<td>13.7</td>
<td>0.0320</td>
<td>0.886</td>
<td>58</td>
<td>1560</td>
<td>0.0151</td>
<td>6.53</td>
</tr>
<tr>
<td>Anular (Regular)</td>
<td>21.3</td>
<td>0.0206</td>
<td>2.829</td>
<td>36</td>
<td>1851</td>
<td>0.0136</td>
<td>7.51</td>
</tr>
</tbody>
</table>

**REFERENCES**


V. CONCLUSION

Since, down flow regime is comparatively very short than up flow regime in any case, so; maximization of mass transfer parameter which gives increase in mass transfer rate for up flow regime will give considerable increase in yield of oil production. Regular shaped of seed holder is always preferred for better extraction yield. Use of annular shaped seed holder gave lower down flow time, higher driving force for up flow regime, higher duration of the period and above all higher $a_x$; resulted higher yield. So, use of effective shape of the seed holder may improve yield of oil production by improving extraction rate.

**B. Equilibrium between Solid and Solvent**

Generally, higher extraction yield is achievable at the start of the process when the pure solvent extracts the free oil originating from the pores of the crushed seed and end of the process, extraction is more difficult probably due to diffusion through the pores [12] and ultimately becomes insignificant. This has also occurred in this study. Lower amount of oil recovery in the solvent was observed with increase of up flow duration. Lower oil production decreases density and viscosity of the oil-solvent mixture which is reflected in Fig. 3 and Fig. 4. Change of density and viscosity with accumulation height in the up flow regime was very prominent in annular shaped seed holder.

Fig. 3. Variation of density of oil-solvent mixture with Accumulation height. Seed Holder Type: Cylindrical, Bed Height: 13.7 cm, Specific gravity of pure 2-propanol: 0.78

Fig. 4: Variation of viscosity of oil-solvent Mixture with accumulation. Height Using Viscometer MAKE: Brookfield viscometer, MODEL: DV-I, with Enhanced UL. Adapter no.: M06-084, Speed 50 rpm
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